



We will serve the customers with the highest quality products

KARAJET® INDUSTRIAL Co.
COMMITTED TO THE HIGHEST EFFICINCY

TEL : 05135413212 FAX : 05135413211
Mashhad, Iran
No. 870, 15 St., Andisheh Blvd., Toos Industrial Estate

Commercial@karajet.com
www.karajet.com

• SPRING HANGER & PIPE SUPPORT

KARAJET® INDUSTRIAL Co.,Ltd

2020 EDITION
**SPRING HANGER
&
PIPE SUPPORT**

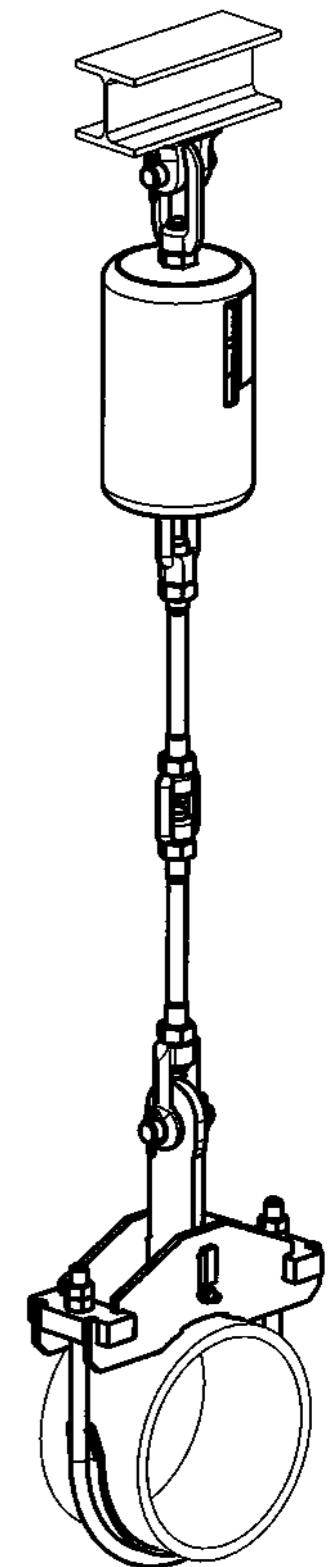
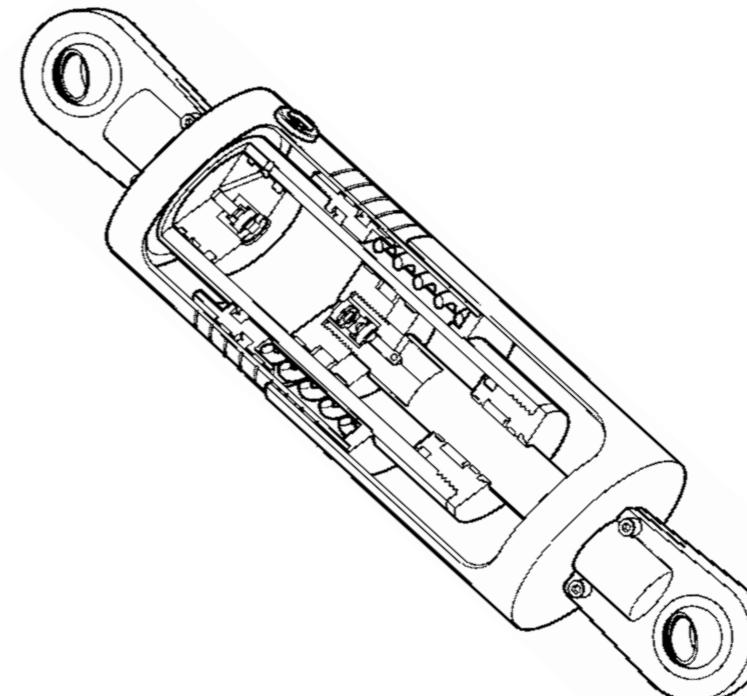
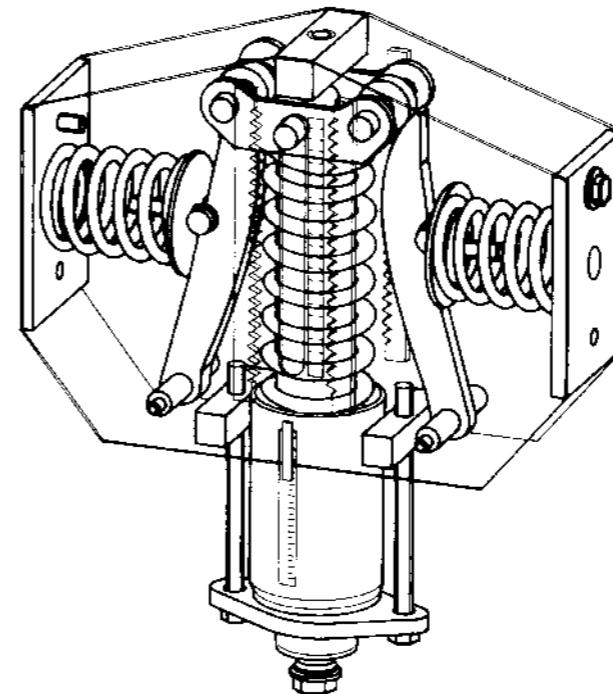


KARAJET® INDUSTRIAL Co.
COMMITTED TO THE HIGHEST EFFICINCY

Contents

01. Variable Springs	5 ~ 10
02. Constant Springs	11 ~ 34
03. Rigid Sway Strut	35 ~ 36
04. Snubber	37~ 46
05. INSTALLATION MANUAL	47 ~52

Advanced technology via introduction of new technology
We will create changes continuously with new idea and creative mind



Pictorial Guide

* Variable Spring Hanger



Type A
page 7



Type B
page 8



Type C
page 9

* Constant Spring Hanger (Horizontal Type)



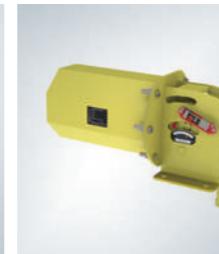
Type A
page 15



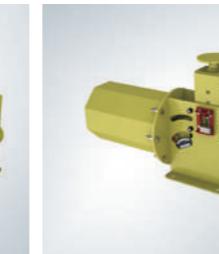
Type B
page 17



Type C
page 19



Type D
page 21



Type F
page 23

* Constant Spring Hanger (Vertical Type)



Type B
page 25



Type C
page 27



Type D
page 29



Type F
page 30

* Constant Triple Spring Hanger



Type A
page 33



Type B
page 34

* Rigid Sway Strut



Rigid Sway Strut A&C
page 36



Rigid Sway Strut B&D
page 36

* Snubber



Snubber-SNA
page 45



Snubber-DA
page 41

Pictorial Guide

* Service

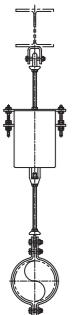
Whenever piping moves vertically, there is a need for a pipe hanger which will support the piping while accommodating the vertical movement. A spring type hanger fills this function. If the movement does not exceed the allowable spring deflection, and if the inherent change in supporting force caused by the spring deflection is allowable, a variable spring fills this function. Simply enough, as the piping moves in a vertical direction, it causes the variable spring to deflect an equal distance. As the spring deflects, the supporting force it is exerting on the pipe changes by an amount equal to the vertical movement times the spring rate. That spring rate is a constant, unique for each size of a particular series. Spring rates are shown at the bottom of the variable spring load chart.

* Adjustment

After the piping or equipment is erected and after all testing which might cause a temporary change in loading conditions is completed, the variable spring should be adjusted to its cold position. This is accomplished by turning the turnbuckle on Types A, B and the load adjusting nut on types C until the position indicator is properly located. If travel stops have been furnished they should be removed prior to equipment operation. After the piping or equipment reaches its full operating conditions, a check and, if necessary, a final adjustment to the hot position should be made at the variable spring.

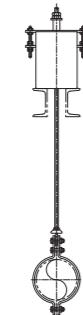
* Selection of a Variable Spring

When choosing a variable spring, a determination of size, model and type must be made. Size and model are chosen jointly based on movement and load considerations as tabulated. The type of spring to be used is normally determined by the physical characteristics of the structure to which the hanger assembly will be attached.



TYPE A

For use where extensive headroom is available and where it may be desirable locate the spring at a specific elevation in the hanger assembly



TYPE B

For use where the spring is to be located on top of a pair of channels and adjustment of the spring is desirable from above the supporting steel



TYPE C

For use when the spring is to be located underneath the piping

* Size and Model Selection

The key criteria in selection the size and series of a variable is a factor known as variability. This is a measurement of the percentage change in supporting force between the hot and cold positions of a spring and is calculated from the formula:

$$\text{Variability} = \frac{\text{Movement} \times \text{Spring Constant}}{\text{Hot Load}}$$

The cold load is calculated by adding (for up movement) or subtracting (for down movement) the product of spring rate time movement to or from the hot load. If an allowable variability is not specified, good practice would be to use 25% for non-critical piping and 10% for critical piping.

Ordering : Specify model name, type and size.

* To Size a Spring, then:

1. Calculate the maximum allowable spring rate from the formula : $\text{Spring Constant} = \frac{\text{Variability} \times \text{Hot Load}}{\text{Movement}}$
2. Determine the size by finding the hot load in the chart.
3. Stay in that size column and choose the series with a spring rate equal or less than the value calculated above.
4. Calculate the cold load and check that both hot and cold loads fall within working range.

$$\text{Cold Load} = \text{Hot Load} \pm (\text{Spring Rate} \times \text{Movement})$$

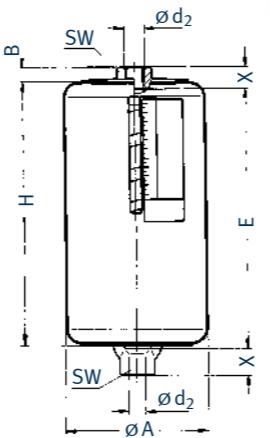
(+ : Moving Up, - : Moving Down)

5. If this condition is not met, move to an adjacent size and rework.

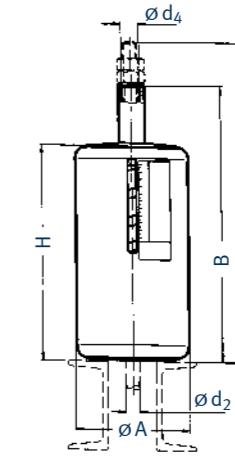
If load, movement, variability, or available space prohibit the use of a variable spring the use of a constant support should be considered.



TYPE-A

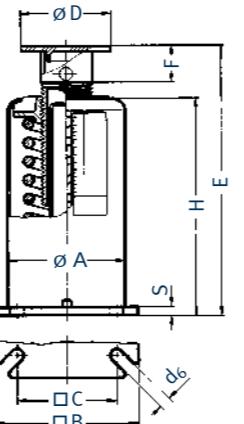


TYPE-B



type	ØA	B	Ød ₂	E①	H	SW	X	weight [kg]
21 C2 19	80	11	M10	205	205	19	15	1.9
21 D2 19	90	11	M10	250	245	19	15	3.0
21 D3 19	90	11	M10	475	470	19	15	5.0
21 11 18	90	11	M12	155	145	19	15	2.1
21 12 18	90	11	M12	250	245	19	15	3.1
21 13 18	90	11	M12	475	470	19	15	5.5
21 21 18	115	12	M12	155	150	19	15	3.8
21 22 18	115	12	M12	255	250	19	15	5.3
21 23 18	115	12	M12	475	460	19	15	8.6
21 31 18	115	13	M16	160	155	24	20	4.3
21 32 18	115	13	M16	255	250	24	20	6.0
21 33 18	115	13	M16	475	470	24	20	9.7
21 34 18	115	13	M16	840	725	24	20	14.0
21 41 18	155	17	M20	185	180	30	25	9.2
21 42 18	155	17	M20	290	290	30	25	12.8
21 43 18	155	17	M20	525	525	30	25	20.0
21 44 18	155	17	M20	920	800	30	25	29.0
21 51 18	180	21	M24	215	215	36	30	16.5
21 52 18	180	21	M24	305	305	36	30	20.5
21 53 18	180	21	M24	540	540	36	30	32.0
21 54 18	180	21	M24	1035	825	36	30	46.0
21 55 18	180	21	M24	1275	1065	36	30	57.0
21 61 18	220	24	M30	245	245	46	35	31.0
21 62 18	220	24	M30	360	360	46	35	40.0
21 63 18	220	24	M30	640	640	46	35	62.0
21 64 18	220	24	M30	1205	980	46	35	90.0
21 65 18	220	24	M30	1490	1265	46	35	114.0
21 71 18	245	30	M36	280	285	55	45	48.0
21 72 18	245	30	M36	405	410	55	45	63.0
21 73 18	245	30	M36	675	680	55	45	89.0
21 74 18	245	30	M36	1300	1070	55	45	133.0
21 75 18	245	30	M36	1575	1345	55	45	160.0
21 81 18	245	30	M42	305	320	65	50	58.0
21 82 18	245	30	M42	470	485	65	50	80.0
21 83 18	245	30	M42	845	860	65	50	126.0
21 84 18	245	30	M42	1430	1330	65	50	182.0
21 85 18	245	30	M42	1810	1710	65	50	228.0
21 91 18	275	36	M48	330	355	75	60	84.0
21 92 18	275	36	M48	505	530	75	60	111.0
21 93 18	275	36	M48	870	895	75	60	164.0
21 94 18	275	36	M48	1515	1395	75	60	243.0
21 95 18	275	36	M48	1885	1765	75	60	296.0

type	ØA	B①	Ød ₂	Ød ₄	H	X _{max} ①	weight [kg]
25 D2 19	90	350	M10	13	245	380	2.8
25 D3 19	90	675	M10	13	470	705	4.9
25 11 18	90	200	M12	13	145	230	2.1
25 12 18	90	350	M12	13	245	380	3.1
25 13 18	90	675	M12	13	470	705	5.5
25 21 18	115	205	M12	13	150	235	3.5
25 22 18	115	355	M12	13	250	385	5.1
25 23 18	115	665	M12	13	460	695	8.4
25 31 18	115	210	M16	18	155	250	3.7
25 32 18	115	355	M16	18	250	395	5.3
25 33 18	115	675	M16	18	470	715	8.9
25 41 18	155	230	M20	25	180	280	8.0
25 42 18	155	395	M20	25	290	445	11.5
25 43 18	155	730	M20	25	525	780	18.6
25 51 18	180	265	M24	28	215	325	14.5
25 52 18	180	405	M24	28	305	465	18.0
25 53 18	180	740	M24	28	540	800	29.0
25 61 18	220	300	M30	34	245	375	26.0
25 62 18	220	465	M30	34	360	540	35.0
25 63 18	220	845	M30	34	640	920	56.0
25 71 18	245	350	M36	40	300	440	40.0
25 72 18	245	530	M36	40	430	620	53.0
25 73 18	245	900	M36	40	700	990	79.0
25 81 18	245	385	M42	47	335	495	44.0
25 82 18	245	605	M42	47	500	715	66.0
25 83 18	245	1075	M42	47	875	1185	111.0
25 91 18	275	415	M48	54	370	535	67.0
25 92 18	275	645	M48	54	545	765	92.0
25 93 18	275	1110	M48	54	910	1230	143.0



TYPE-C

type ②	ØA	ØB	ØC	d ₆	E ① ②	F	H	ØD	S	weight [kg]
29 C2 19	80	105	75	10	270	36	210	80	6	2.6
29 D1 19	90	125	95	12	195	36	145	80	8	3.2
29 D2 19	90	125	95	12	305	36	245	80	8	4.3
29 D3 19	90	125	95	12	550	36	470	80	8	6.6
29 11 18	90	125	95	12	195	36	145	80	8	3.4
29 12 18	90	125	95	12	305	36	245	80	8	4.6
29 13 18	90	125	95	12	550	36	470	80	8	7.2
29 21 18	115	150	115	14	200	36	150	100	10	5.6
29 22 18	115	150	115	14	310	36	250	100	10	7.6
29 23 18	115	150	115	14	540	36	460	100	10	11.1
29 31 18	115	150	115	14	205	36	155	100	12	6.3
29 32 18	115	150	115	14	310	36	250	100	12	8.4
29 33 18	115	150	115	14	550	36	470	100	12	13.0
29 41 18	155	190	140	18	240	48	180	120	12	11.9
29 42 18	155	190	140	18	360	48	290	120	12	16.0
29 43 18	155	190	140	18	615	48	525	120	12	25.0
29 51 18	180	220	170	18	270	50	210	150	12	20.0
29 52 18	180	220	170	18	370	50	300	150	12	24.3
29 53 18	180	220	170	18	625	50	535	150	12	37.0
29 61 18	220	260	200	23	305	50	245	170	15	34.0
29 62 18	220	260	200	23	430	50	360	170	15	44.0
29 63 18	220	260	200	23	730	50	640	170	15	68.0
29 71 18	245	290	215	23	360	52	300	200	20	53.0
29 72 18	245	290	215	23	500	52	425	200	20	68.0
29 73 18	245	290	215	23	790	52	695	200	20	97.0
29 81 18	245	290	215	27	400	55	335	200	20	60.0
29 82 18	245	290	215	27	575	55	500	200	20	84.0
29 83 18	245	290	215	27	965	55	870	200	20	133.0
29 91 18	275	340	255	33	440	60	370	240	25	91.0
29 92 18	275	340	255	33	625	60	545	240	25	118.0
29 93 18	275	340	255	33	1010	60	910	240	25	173.0

Model : CHH (Horizontal), CHV (Vertical)

Constant springs are used where vertical movements should not be restricted by rigid hangers and where variable spring can not be used due to the high deviation between installation load and operating load. The less the load variability factor of a hanger is, the less the reaction effects on equipment or pipe systems due to thermal expansion.

In case variability factor is variable according to vertical movement and acting load. Therefore, it is called "Variable" spring. It is often the case that the vertical movement or reaction force is so large that variable springs can not be used.

The load variability of constant spring is theoretically zero and, therefore, this type of spring hanger is capable of supporting a pipe with a constant load at any time, in spite of the position of vertical movement during operation or shutdown condition. Therefore, it is called "Constant" spring.

KARAJET's constant spring assures perfectly support through the entire deflection of the pipe load. This counter-balancing of the load and spring moments about the main pivot is obtained by the use of carefully designed compression type load springs, lever and spring tension rods.

* Selection of a Constant Spring

When choosing a constant spring, a determination of size, model and type must be made.

To select the size, determine the total to be supported by the constant spring as well as actual vertical movement of the pipe at the point of supporting location.

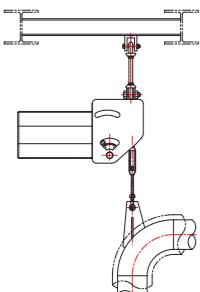
Total travel should be equal to actual travel plus 20% plus 20mm.(Total Travel=Actual Travel x 1.2+20mm)

Total travel is the maximum vertical movement the constant spring can accommodate.

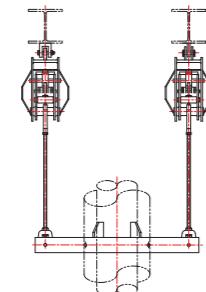
Select a size which will accommodate the and actual from Load-Travel chart on pages 22 and 23.

To determine constant spring model and type, consideration of available room for suspending the pipe and spring will indicate which model and type of constant spring is desirable.

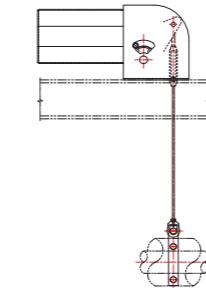
* CHH (Horizontal)



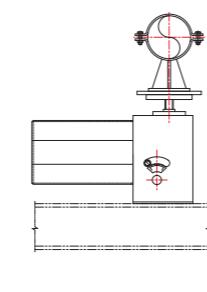
TYPE A



Type B & Type C

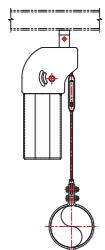


Type D

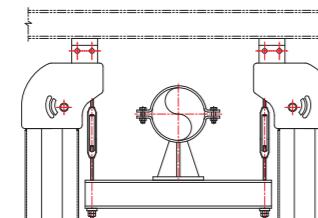


Type F

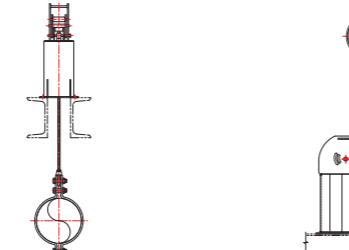
* CHV (Vertical)



Type B



Type C



Type D



Type F

The type of spring to be used is normally determined by the physical characteristics of the structure to which the hanger assembly will be attached. The usage of each type is the same as variable springs.

* Field Adjustment

When the hanger is installed, its supporting force should be in balance with the portion of the piping weight assigned to it. Each hanger is individually calibrated before shipment to support to exact load specified.

Therefore, there is no need to adjust the springs at erection field in general. In spite of that, special instructions for this field recalibration of spring may be obtained from KARAKET engineer.

No less than 10% of this adjustability is provided either side of the calibrated load for field adjustment.

The load adjustment is made by turning the single load adjustment bolt.

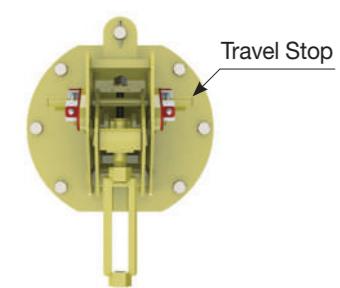
* Travel Stop

The functional design of the constant spring permits the incorporation of a travel stop that will lock the hanger against upward or downward movement for temporary conditions of under load or overload, such as may exist during erection, hydrostatic test or chemical clean-out.

The travel stop is inserted through the opening made on the side frame and inside load arm.

This travel stop is designed to bear two times of calculated load in consideration of overloads due to hydrostatic test condition.

Assure not to remove travel stop unless hydrostatic test is completed.



* Universal Locking Type

In order to reset constant springs different from original setting in accordance with special condition, KARAJET also provides Universal locking type constant springs equipped with special travel stop. This travel stop consists of two plates, with matched serrations, attached to the hanger side frame with two or more cap screws and with a socketed piece which engages the position indicator. A series of serrations can be engaged to lock the hanger at any position along the total travel range. The travel stop must be removed before the piping system is put into operation, but not before the hanger is fully loaded. The travel stop is released by removing the cap screws.



* Corrosion - Resistant Type

KARAJET also can provide Corrosion - Resistant type of constant spring or protection against severe or corrosive condition like variable springs.

These springs are provided with neoprene or CIP coated spring coils and hot-dipped galvanized metal parts except threaded load column for type F which is electro-galvanized.

Triple Type

* Service

Minor thermal displacement in the pipe systems in the vertical direction can be compensated by spring supports or spring hangers. Due to the resulting proportionally increasing force deviation corresponding to the spring rate, their use is limited to a displacement range specified by the designer.

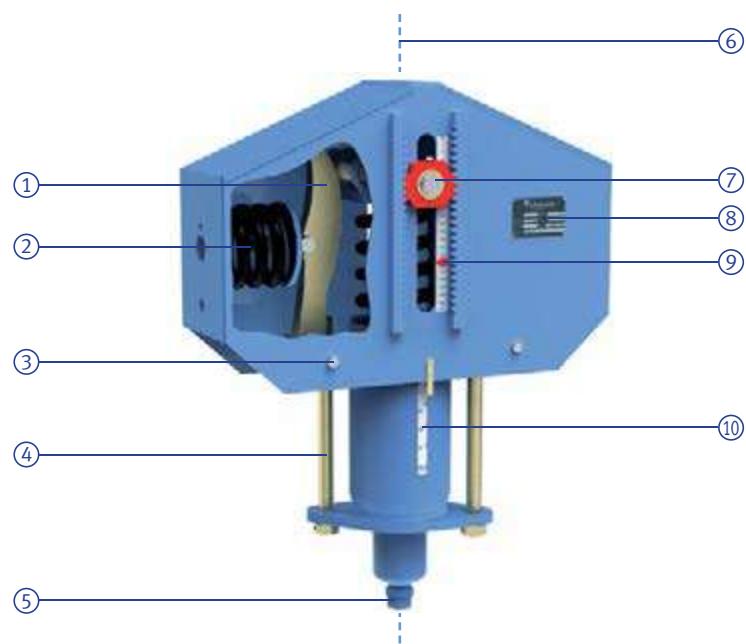
In the case of greater vertical displacement the use of constant hangers or constant supports is required.

For these special designs, the spring force is transformed into a constant force throughout the displacement range. The proportional loads of the pipe system can in this way be constantly distributed over the whole displacement range without significant deviations.

The function principle is based on the arrangement of three springs resulting in the parallelogram of forces.

The design is distinguished by highly functional accuracy along with wide load adjustment ranges.

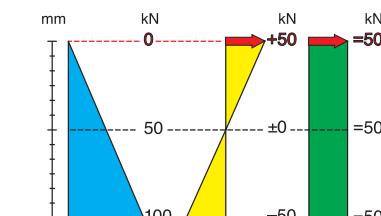
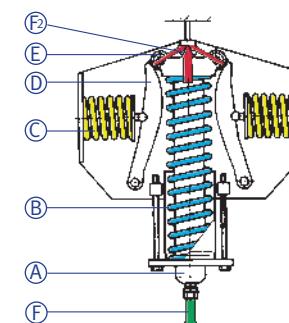
The favorable performance-to-weight ratios and symmetrical designs enable easy installation.



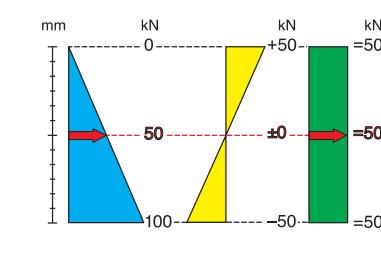
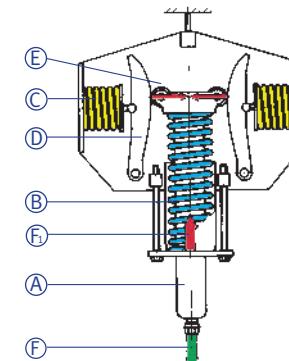
* Feature

- 1) Principle-based constancy by way of a special function principle.
- 2) Pre-relaxed springs eliminate any significant loss of load-bearing capacity.
- 3) Reduced friction due to minimized number of bearing points.
- 4) Especially wide load adjustment range avoids hanger replacement when operational loads change.
- 5) Turnbuckle and swivel joint function allows greater adjustment of pipe installation position.
- 6) Load application free of moments due to a single suspension point.
- 7) Blocking device through fine rasterization nearly infinitely variable.
- 8) Name plate contains complete technical specifications.
- 9) Directly readable travel scale with marking for hot/cold positions.
- 10) Load scale with permanent marking of set load.
- ✓ Symmetrical design ensures direct flow of forces through axis of symmetry.
- ✓ Favorable performance-weight ratios for reduced installation loads.
- ✓ Arranged by load groups and travel ranges to simplify selection (modular system).
- ✓ Consistent functional behavior due to highquality corrosion protection and maintenance-free chemically nickelized finishes.
- ✓ Readily adaptable to installation situation via corresponding designs and standardized accessories.
- ✓ Double load-tube guiding of constant supports for transmission of side loads.
- ✓ Secure connection of load chains due to load- and connection-compatible modular components.

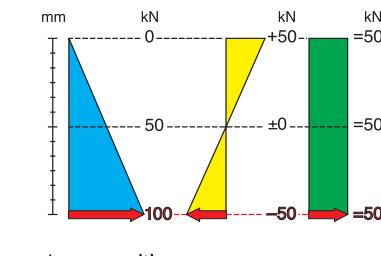
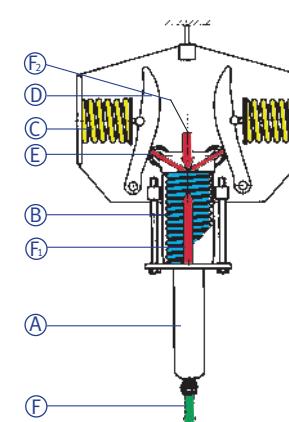
Triple Type



Upper position



Middle position



Lower position

The KARAJET Function Principle is based on the interaction of the force from a mainspring and the resulting force of two connected balance springs. The force directions of the pre-loaded compensating springs are thereby angled against each other in the shape of a parallelogram of forces.

The suspended load (F) acts directly on the mainspring (B) via the load tube (A). The pre-loaded compensating springs (C) act additionally on the load tube as the resulting force (F) via pivoting cams (D) and roller supports (E). The mainspring force (F) and the resulting force (F) change on the shifting of the load over the displacement range in accordance with the specified spring constants, the cam path, and the angular position of the cam components.

The course of the resulting force corresponds to the characteristics of the mainspring. In this way the mainspring force is balanced out, without deviations, to a constant support force.

- The KARAJET function principle leads to absolute constancy which by theory can easily be proven.
- The KARAJET function principle permits an especially wide load adjustment range of 40% – 100% of the nominal load.

Rigid Sway Strut

Model : RSS-A, RSS-B, RSS-C, RSS-D

* Service

Sway struts are used to restrain movement of piping in one direction while providing for movement due to thermal expansion or contraction in another direction.

* How to select

Select size consistent with max. recommend. load to be restrained. The load indicated in the table represents the value under normal operation condition.

Determine "L" dimension and check to be within limits of min. and max. "L" dimension listed for size selected.

For restraint parallel to the pipe axis using two sway strut assemblies, a riser clamp is available. However, if a riser clamp is required, consult KARAJET engineer for information about this clamp.

* Installation

Shipped assembled. Securely fasten bracket to structure, make necessary adjustment in overall length and fasten clamp to pipe.

* Feature

- Effective under either or compressive force.
- Provides 90mm(Type A&C) or 50(Type B&D) of field adjustment in either direction.
- Self-aligning bushings permit $\pm 5^\circ$ misalignment or angular motion. Bushings are coated with a dry lubricant.
- Almost no mechanical gap.

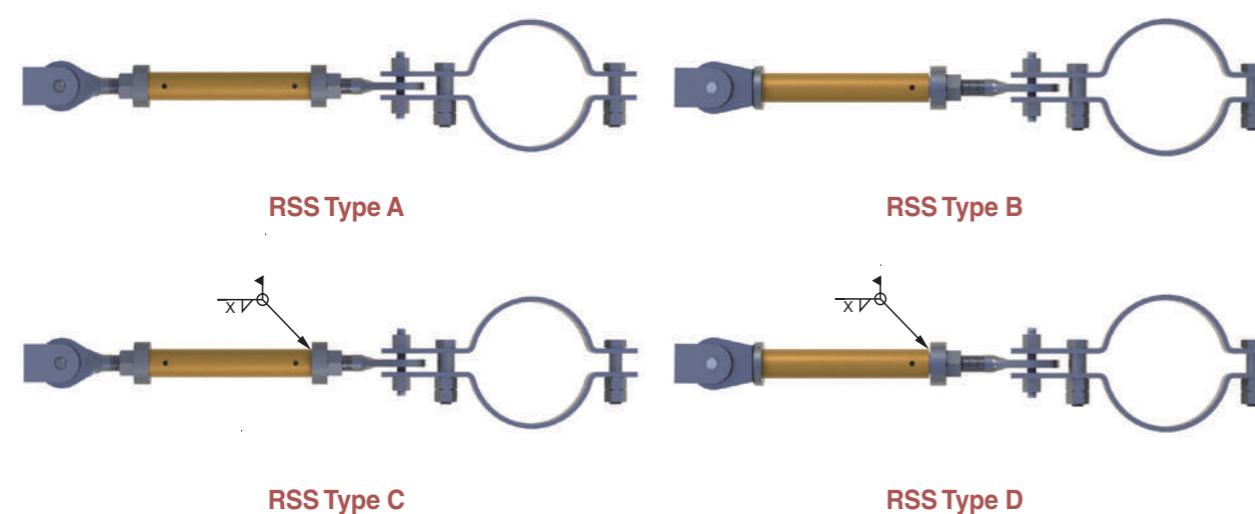
* Ordering

Specify model name, type, size and pin-to-pin length(L).

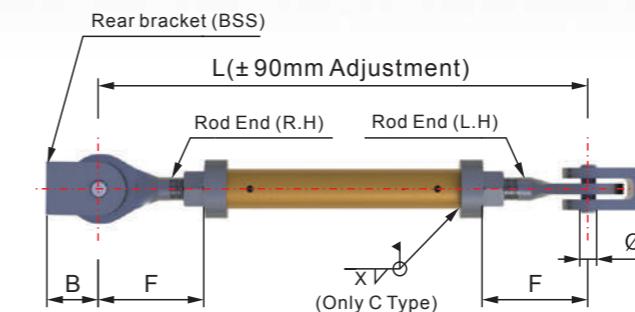
Alloy or stainless steel pipe clamps are available as a special order.

The rear bracket assembly can be ordered separately.

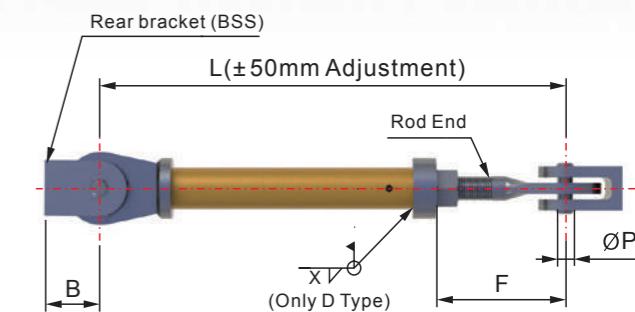
ex) RSS - A - 5 x 1500L



Rigid Sway Strut



RSS A & C Type



RSS B & D Type

Size	Rod End	Extension Pipe	B	F	$\emptyset P$ (nom.)	Min. L		X
						A & C	B & D	
1	M20	25A(Sch.80)	45	165	12.5	590	354	6
2	M24	50A(Sch.40)	55	170	19	630	377	6
3	M30	50A(Sch.160)	65	195	25	710	423	9
4	M36	65A(Sch.160)	65	200	25	720	431	9
5	M42	65A(Sch.160)	80	245	31.5	810	495	9
6	M56	80A(Sch.160)	125	270	38	870	543	13
7	M64	100A(Sch.160)	145	300	44	960	602	13
8	M72	100A(Sch.160)	160	340	50.5	1080	695	16
9	M80	100A(Sch.160)	160	345	50.5	1090	700	19
10	M100	150A(Sch.160)	205	460	69.5	1380	898	25

Loads must not be applied outside a 10° included angle cone of action to the pipe clamp axis without special authorization.

* Max. Recommended Load (kg)

Size	"L" Dimension																
	250	500	750	1000	1250	1500	1750	2000	2250	2500	2750	3000	3500	4000	4500	5000	5500
1	1220	1220	1220	1220	1220	1180	900	720	-	-	-	-	-	-	-	-	-
2	2250	2250	2250	2250	2250	2250	2100	1630	1350	1100	900	-	-	-	-	-	-
3	3600	3600	3600	3600	3600	3600	3270	2630	2130	1770	1450	1220	-	-	-	-	-
4	5250	5250	5250	5250	5000	4750	4750	4250	4000	3750	3500	3250	-	-	-	-	-
5	7100	7100	7100	7100	7100	7100	7100	6800	6000	5000	4000	3500	2600	2000	-	-	-
6	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	12300	11000	9300	7000	-	-	-
7	-	15200	15200	15200	15200	15200	15200	15200	15200	15200	15200	14200	11600	9000	7200	5850	4800
8	-	23000	23000	23000	23000	23000	23000	23000	23000	23000	23000	23000	20000	17500	14500	12000	10000
9	-	-	31000	31000	31000	31000	31000	31000	31000	31000	31000	31000	31000	31000	31000	28000	25000
10	-	-	55000	55000	55000	55000	55000	55000	55000	55000	55000	55000	55000	55000	55000	55000	45000

Hydraulic Snubber

Model : DA

The snubbers are linear supports designed to limit unwanted sudden movements of components such as :

- Pipes
- Tanks
- Control valves
- Steam generators
- Safety valves
- Pumps, motors etc.

The snubbers enable slow movements due to thermal dilatation in both directions and oppose only low resistance to such movements.

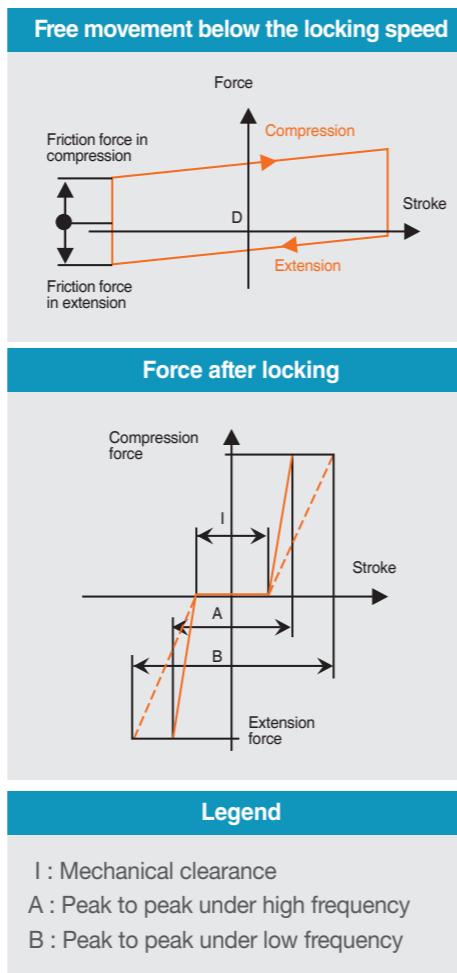
But when the movement speed leads to dynamic displacement that are harmful to the installation, the snubbers are immediately locked at the desired speed and support the dynamic force by transferring it to the fixed structure.

Once the disturbance has passed, the device returns to its initial state and enables slow movements once again.

In that way, the snubbers provide temporary additional support to the installation in order to prevent it from entering into resonance, thereby minimising the risk of breaking due to vibrations.

The snubbers therefore prevent damage due to:

- Earthquakes
- Water hammer effects
- Violent thrusts due to safety valve discharge or breaks in piping
- Wind
- Other similar disturbances

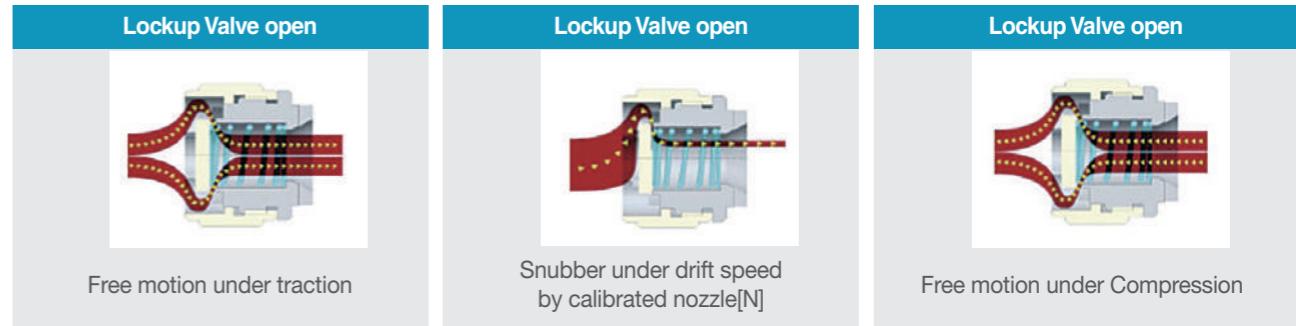


* Valve

Lockup valve defining the lockup velocity are tested one by one in our factory. Nozzles are designed and sized to be independent from the fluid viscosity and temperature. KARAJET is using a Self Cleaning Lockup Valve.

The self cleaning lockup valve (SCLV) ensures 2 functions : blocking and drift. The integration of both function is made by machining a «V» shape slit on the working area of the valve so that :

- The SCLV is never totally closed to assure the decompression
- After drift through the «V» shape slit, the pressure will decrease and allows the opening of the valve. This process ensures the self cleaning of the valve comparing to a classic nozzle which would be definitively stopped in case of impurity contains in the oil. With this technology, we can realize very low drift speed without risk to plug the nozzle.



* Snubber selection criteria

Dynamic load :

At the nominal load FN, Check that the snubber is capable of handling dynamic forces during normal operation and/or operating basis earthquake conditions (level A/B). In the upset situation, check that the snubber is capable of handling the forces expected at level D, safe shutdown earthquakes.

Stroke :

The selected snubber must be able to make the fixing points cover the maximum travel between the assembly position and extreme operating position. Users should select the snubber with a minimum margin of 10 mm is available in the assembly position.

►► A travel indicator on the body's snubber allows to verify the good operation position.

Available space :

Make sure that when the snubber is in place, the expected movements are possible with the minimum margins. Add an extension if the space available is larger than travel capability of the snubber.

►► The snubber may be assembled in either direction. Make sure that the spherical bearings can move freely, in the assembly position and in the operating position.

* Raw materials

Tempered stainless steel rod with chemical nickel coating
Tempered stainless steel eye ends
Body an internal parts in high quality carbon steel

* Dynamic characteristics at ambient temperature, 15°C to 20°C

Operating from 0.5 up to 100 Hz with symmetrical compensation system and internal pressurising.

Hydraulic Snubber

Model : DA

* Locking speed :

2 mm/s to 6 mm/s or as requested

* Friction force at slow speeds, before locking

$f < 500\text{N}$ if $\text{FN} \leq 30\text{kN}$

$f < 2\%$ FN if $\text{FN} < 200\text{kN}$

$f < 1\%$ FN if $\text{FN} \geq 200\text{kN}$

* Drift speed after locking,

at FN : 0.1 mm/s to 2.0 mm/s or as requested

* Peak-to-peak movement under sinus alternating load FN from 3 to 33 Hz

< 4 mm if $\text{FN} \leq 100\text{kN}$

< 5 mm if $\text{FN} \leq 600\text{kN}$

< 6 mm up to FN = 600 kN

* Environment conditions

Temperature :

Normal service temperature : - 20°C to + 80°C

Minimum storage temperature : - 30°C

Humidity :

100 %

External pressure :

Service pressure : 1 bar

Accidental pressure : 5 bar

Total dose of Y rays and neutrons : 60 Mrad

* Stiffness

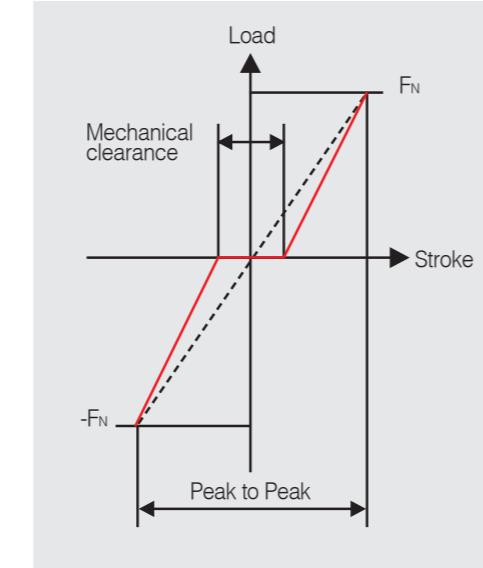
Snubber stiffness is defined according to the following diagram where :

FN is the Nominal load of the snubber **Peak to Peak** the Total stroke under alternative load, and **Snubber Stiffness** is :

$$K = \frac{2 \times \text{FN}}{\text{Peak}}$$

Model	Nominal load (kN)	Stroke (mm)	Stiffness* (kN/mm)
DA1	14	100	13
		200	11
DA2	30	150	23
		300	16
DA3	47	150	33
		300	25
DA4	100	150	69
		300	47
DA5	200	150	124
		300	76

*Tolerance on stiffness value : ± 25%



* Permissible load in kN

The permissible load in terms of dynamic stress in the table below has been calculated in accordance with cod RCCM vol. H level S1 and is valid for snubbers and fastening accessories –weld-on bracket, pins, extensions.

Model	Total stroke (mm)	FN load level A/B/80°C (kN)	Emergency load Level C/80°C (kN)	Faulted load Level D/150°C (kN)
DA1	100, 200	14	18	24
DA2	150, 300	30	39	49
DA3	150, 300	47	62	77
DA4	150, 300	100	133	140
DA5	150, 300	200	266	280
DA6	150, 300	320	425	545
DA7	150, 300	600	798	1020
DA8	150, 300	1100	1463	2000
DA9	120	-	-	3500
DA10	100	-	-	4500
DA11	100	-	-	6500
DA12	100	-	-	8500

* Load definition :

Normal/Disturbed - Level A/B : Nominal load (FN) including dynamic stress due to normal operation and operating basis earthquakes.

Emergency - Level C : Dynamic loads except normal functioning as well as the safety earthquakes.

Faulted - Level D : Dynamic loads in accidental situations, including safe shutdown earthquakes (SSE).
The snubbers should undergo verification as a minimum after such an event.

* Life under dynamic stress

The snubbers may be subject to the total dynamic loads below, without any adverse effect on operating, at atemperatur ≤ 80° C.

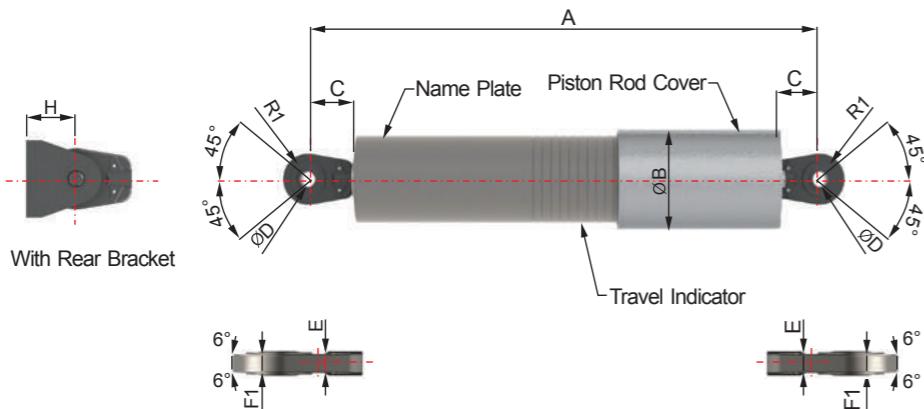
Load (in % FN)	Number of cycles
10%	5×10^6
50%	10^6
100 % (level A/B)	10^5
133 % (level C)	10^3
(level D)	10^2

* Large Bore - Technical characteristics

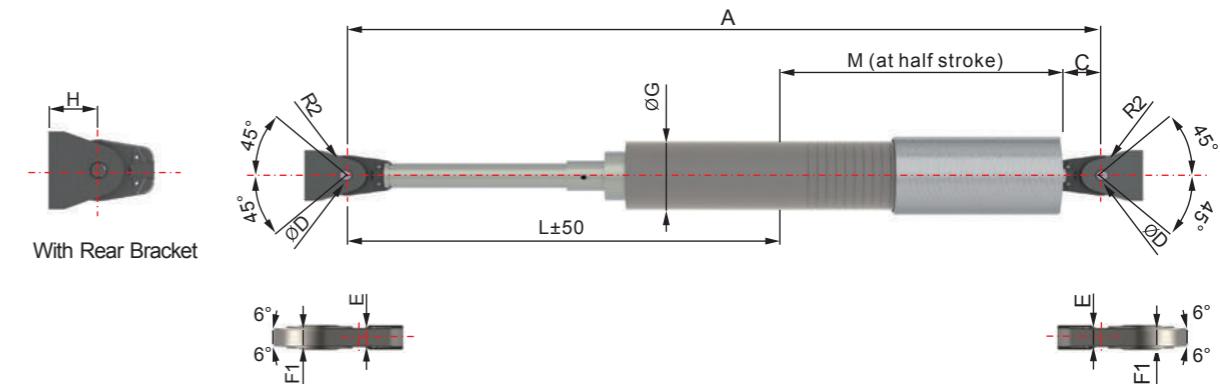
- drag force : < 15 kN (DA12)
- lockup velocity : 6 mm/min < LV < 60 mm/min
- drift speed : < 10 mm/min under maximal load
- lost motion : < 1 mm
- theoretic stiffness in traction : > 1200 kN/mm under maximum load (DA12)
- theoretic stiffness in compression : > 1500 kN/mm under maximum load (DA12)
- fluid : Silicon Oil
- functional temperature : 10°C to 60°C

Hydraulic Snubber

Model : DA



Type : Small Bore Snubber



Type : Extension With adjustable Snubber

Type	Nominal load Level B (kN)	Faulted load Level D (kN)	Stroke (mm)	A min (mm)	A half stroke (mm)	A max (mm)	Ø B (mm)	C (mm)	Ø D (mm)	E (mm)	F1°	H (mm)	R1 (mm)	Weight (kg)
DA1-100	14	24	100	435	485	535	102	50	17	20	19	44	28	12
DA1-200	14	24	200	618	718	818	102	50	17	20	19	44	28	16
DA2-150	30	49	150	555	630	705	115	50	20	25	23	44	28	21
DA2-300	30	49	300	845	995	1145	115	50	20	25	23	44	28	30
DA3-150	47	77	150	545	620	695	154	60	25	28	28	50	32	33
DA3-300	47	77	300	795	945	1095	154	60	25	28	28	50	32	46
DA4-150	100	140	150	590	665	740	170	70	30	32	30	62	39	49
DA4-300	100	140	300	850	1000	1150	170	70	30	32	30	62	39	66
DA5-150	200	280	150	710	785	860	220	105	45	43	40	85	58	82
DA5-300	200	280	300	980	1130	1280	220	105	45	43	40	85	58	106
DA6-150	320	545	150	700	775	850	-	68	45	43	40	90	75	120
DA6-300	320	545	300	986	1136	1286	-	68	45	43	40	90	75	160

► Technical Characteristics : see pages 50~53

► Other load, or stroke or characteristic on demand - Bracket & clamps with axis on demand.

Type	Nominal load Level B (kN)	Faulted load Level D (kN)	Stroke (mm)	A max at half stroke (mm)	M at half stroke (mm)	Ø G (mm)	L min (mm)	L max (mm)	C (mm)	Ø D (mm)	E (mm)	F1 (mm)	F2 (mm)	H (mm)	R1 (mm)	R2 (mm)	Weight	
																	L min (kg)	+ per 50mm (kg)
DA1-100	14	24	100	1000	432	40	190	540	50	17	20	19	13	44	28	26.5	2	0.22
DA1-200	14	24	200	1000	665	40	190	340	50	17	20	19	13	44	28	26.5	2	0.22
DA2-150	30	49	150	1400	577	60	200	800	50	20	25	23	17	44	28	32	2.5	0.34
DA2-300	30	49	300	1400	942	60	200	450	50	20	25	23	17	44	28	32	2.5	0.34
DA3-150	47	77	150	1700	557	80	220	1120	60	25	28	28	19	50	32	36.5	4	0.46
DA3-300	47	77	300	1700	882	80	220	820	60	25	28	28	19	50	32	36.5	4	0.46
DA4-150	100	140	150	2100	592	100	250	1500	70	30	32	30	21	62	39	41	10	1.1
DA4-300	100	140	300	2100	927	100	250	1150	70	30	32	30	21	62	39	41	10	1.1
DA5-150	200	280	150	2100	667	120	260	1410	105	45	43	40	30	85	58	56	15	1.4
DA5-300	200	280	300	2100	1022	120	260	1060	105	45	43	40	30	85	58	56	15	1.4

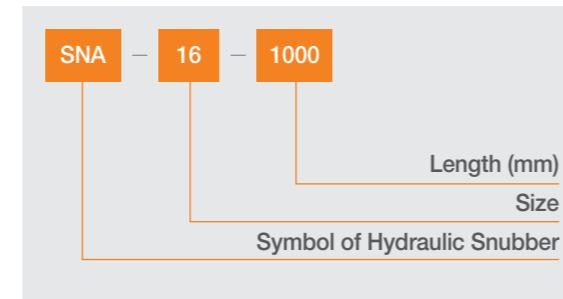
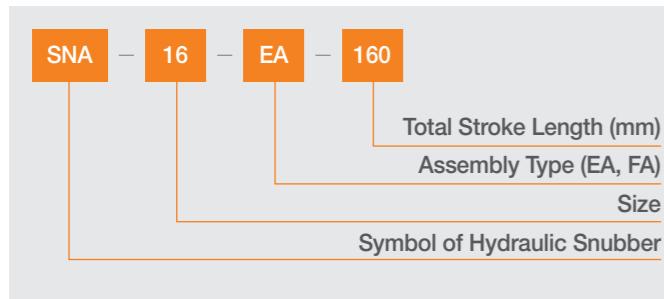
► Length of extension available every 50 mm from L min.

► Adjustment ± 50mm

► Rigid strut on demand

Hydraulic Snubber

Model : SNA



Total Stroke for Snubber(mm)

100(mm), 160(mm), 250(mm) - Standard Type

310(mm), 400(mm), 460(mm) and 510(mm) - Extra stroke ; available on request

Combination of total stroke and design displacement

Design	Total stroke (mm)			
	displacement	100	160	250
50 or less	O	△	△	
51 - 110	X	O	△	
111 - 200	X	X	O	

O : Optimum
△ : Usable
X : Not Usable

* Assembly Type for Snubber

Type FA : with shortest attachment for a limited installation length

Type EA : with extension attachment for a long installation length

For Type EA, snubber extension will be required to enlarge the C-C dimension

* Feature

Show the schematic diagram main items of the Snubber

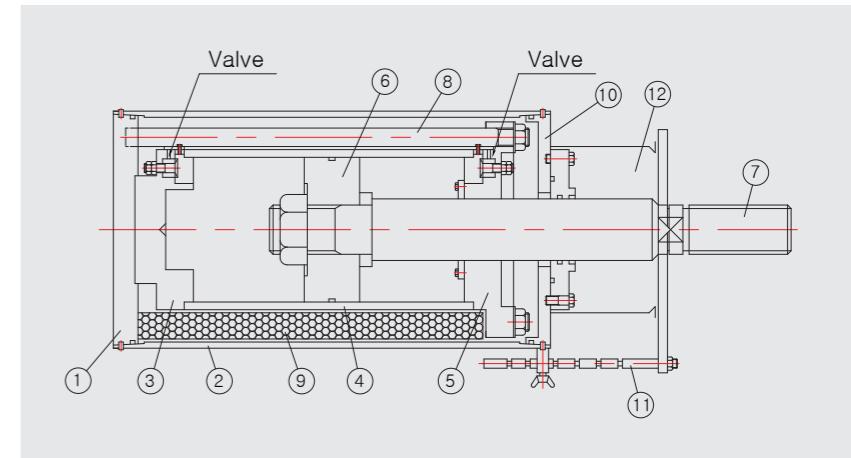
Several features are described as follows;

- (1) Reliable hydraulic system including precise valve mechanism assures stable and symmetrical performance in both loading directions.
- (2) Self-contained oil reservoir eliminates fluid leakage from sealed connections.
- (3) High durability of seal materials longer service duration without frequent maintenance work.
- (4) Well-engineered construction simplifies disassembling and re-assembling of the unit, assuring easier maintenance works.
- (5) Installable in a limited space because of a plain cylinder contour.
- (6) Filled with thoroughly verified genuine hydraulic fluid.
- (7) Easy-to-read stroke indicator.

Caution : Without special comments of the Customer, the snubber will be preset at the shop as follows;

- Preset at 25(mm) if snubber were extended during hot state.
- Preset at [total stroke-25](mm) if snubber were retracted during hot state.

Part NO.	Item Name
1	Holder
2	Casing
3	Cylinder Cover
4	Cylinder Tube
5	Rod Cover
6	Piston
7	Piston Rod
8	Tie Rod
9	Accumulator
10	Casing Cover
11	Travel Indicator
12	Canvas Cover



* Assembly Type for Snubber

Minimum spring rate (kg/mm) per load stroke

Type \ Stroke(mm)	100	160/250
SNA-03	250	150
SNA-06	450	300
SNA-1	650	450
SNA-3	1500	1000
SNA-6	3000	2000
SNA-10	5000	3000
SNA-16	7000	4500
SNA-25	8000	6500

Design Parameters

Design Parameter	Criteria
Drag Force	2% of the rated load, or 50(kg) whichever is greater
Bleed Rate	0.5 (mm/sec)
Lock-up Rate	1~4 (mm/sec)
Frequency Range	1~33 (Hz)
Pressure Capacity	1.5 time of the rated load
Perm. Cycle under rated load	20000 (cycles)
Temperature	-15~60(°C)
Radiant Limit	1*10 (TEKOHR 200 Fluid)
Recommended Maintenance	Once every 10 years
Angular Offset	Max.153°

VARIABLE SPRING

* Installation

- In order to avoid a wrong installation, an identification check must be performed by confirming the Hanger Identification No., Hanger Type and Size carved on the Name Plate attached on the Hanger's side.
- Weld the structural attachments, such as Beam Attachment, Lug Plate or Washer Plate to the steel structure as indicated on the hanger drawings approved by customer.



- Connect the pipe attachments(Pipe Clamp) to the pipe in accordance with the approved hanger drawings.

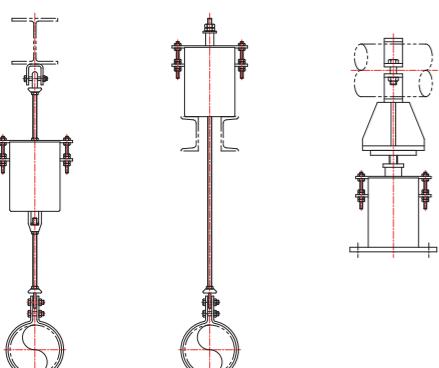


- Assemble the hanger rods and other components to the pipe attachment and Turn buckle of Variable Spring Hanger in accordance with the hanger drawing.



* Attachment of Variable Spring

- Type A, B
Connect the Variable Spring Hanger to the structural attachment using wire or chain block in order to connect it easily.
- Type C
Locate the Variable Spring Hanger at the correct position and weld or bolt it in accordance with the instructions specified on the hanger drawings.



Type A

Type B

Type C

* Travel Stop-Locking Device

- The Variable Support Hangers are normally furnished with travel stops either at near the top or bottom position.

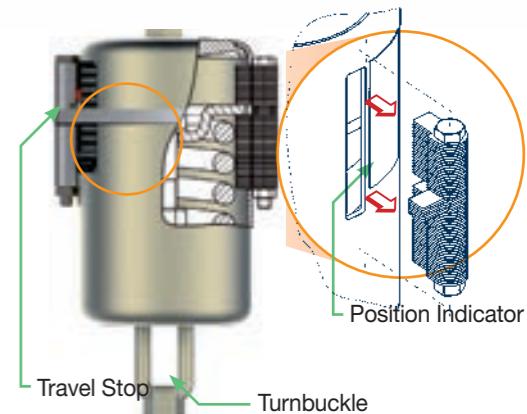
Therefore, at this stage the travel indicator points to the blue("COLD" mark) scale.

These travel stops are provided for making the installation work easy and to lock the hanger against upward and/or downward deflection during installation or hydrostatic test of piping system.

It is normally installed at the factory to hold the hanger in the "COLD" position.

With travel stops in place, the hanger can be used as a rigid support during pipe erection.

Turn the turnbuckle to raise or lower the pipe to the proper elevation.

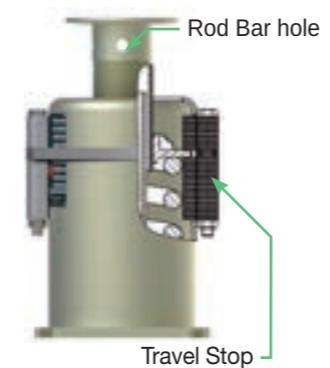


* Travel Stop-Unblocking-Hanging Type

- When finished Hydro-test or steam blowing test, remove the upper and lower straps which move to wanted position.
- After removing Blocking, confirm that Travel Indicator indicates the Cold Marking position. If not, turn the Turnbuckle until the Travel Indicator is on the Cold Marking position.
- When operation, the Position Indicator move to "HOT" position.

* Travel Stop-Unblocking-Support Type

- When finished Hydro-test or steam blowing test, remove the upper and lower Straps which move to wanted position.
- After removing Stop Nut, confirm that Travel Indicator indicates the Cold Marking position.
- When operation, the Position Indicator move to "HOT" position.
- If the Position indicator is not located at the designed position "COLD" or "HOT" it should be adjusted by turning the Load Flange. (By use of the appropriate "Rod bar")



CONSTANT SPRING

* Installation

- In order to avoid a wrong installation, an identification check must be performed by confirming the Hanger Identification No., Hanger Type and Size carved on the Name Plate attached on the Hanger's side.
- Weld the structural attachments, such as Beam Attachment, Lug Plate or Washer Plate to the steel structure as indicated on the hanger drawings approved by customer.



- Connect the pipe attachments(Pipe Clamp) to the pipe in accordance with the approved hanger drawings.

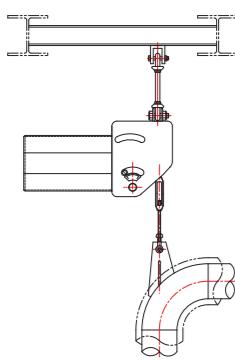


- Assemble the hanger rods and other components to the pipe attachment and Turn buckle of Constant Spring Hanger in accordance with the hanger drawing.

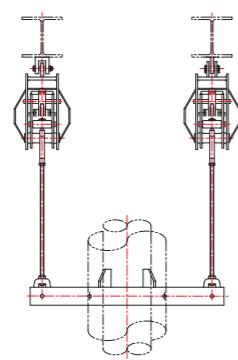


* Attachment of Variable Spring

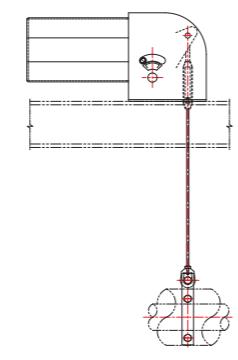
- Type A, B & C
Connect the Constant Spring Hanger to the structural attachment using wire or chain block in order to connect it easily.
- Type D & F
Locate the Constant Spring Hanger at the correct position and weld or bolt it in accordance with the instructions specified on the hanger drawings.



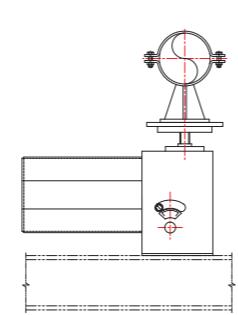
Type A



Type B & C



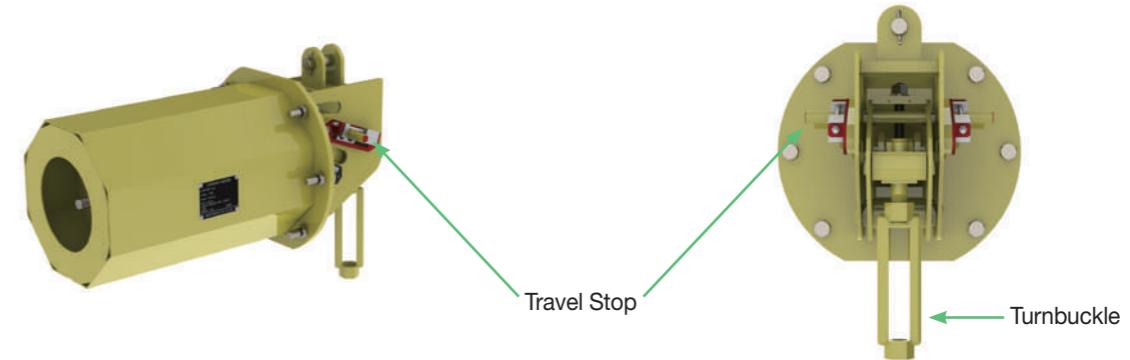
Type D



Type F

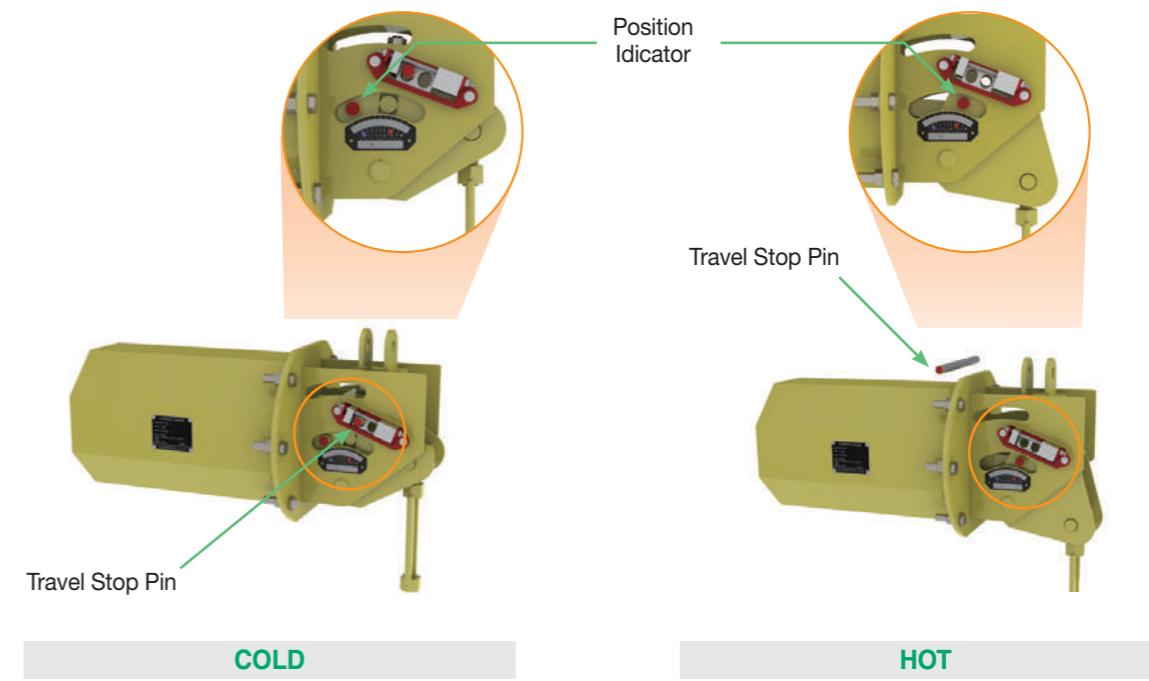
* Travel Stop-Locking Device - Standard Type

- The Constant Support Hangers are normally furnished with travel stops either at near the top or bottom position. Therefore, at this stage the travel indicator points to the blue marker . These travel stops are provided for making the installation work easy and to lock the hanger against upward and/or downward deflection during installation or hydrostatic test of piping system. It is normally installed at the factory to hold the hanger in the "COLD" position. With travel stops in place, the hanger can be used as a rigid support during pipe erection. Turn the turn buckle to raise or lower the pipe to the proper elevation.



* Travel Stop-Unblocking-Standard Type

- Before operation, remove the Travel Stop Pin and release the Travel Stop Nut then Position Indicator move to "HOT" position when operation.



* Travel Stop-Locking Device-Universal Type

1. The Constant Support Hangers are specially furnished with travel stops either at near the top or bottom position.

Therefore, at this stage the travel indicator points to the blue marker.

These travel stops are provided for making the installation work easy and to lock the hanger against upward and/or downward deflection during installation or hydrostatic test of piping system. It is normally installed at the factory to hold the hanger in the "COLD" position.

With travel stops in place, the hanger can be used as a rigid support during pipe erection.

Turn the turn buckle to raise or lower the pipe to the proper elevation.

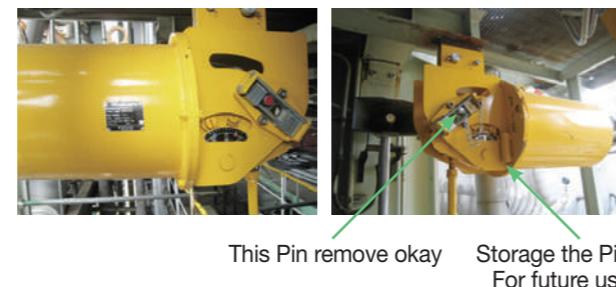


* Travel Stop-Locking Device-Universal Type

<Notice>

Remove(Pulling) the Pin which connected the Chain.

Removed the Pin store the Pin Storage for future use



* Travel Stop-Unblocking-Universal Type

1. Before operation, remove the Travel Stop Pin and release the Travel Stop Nut then Position Indicator move to "HOT" position when operation.

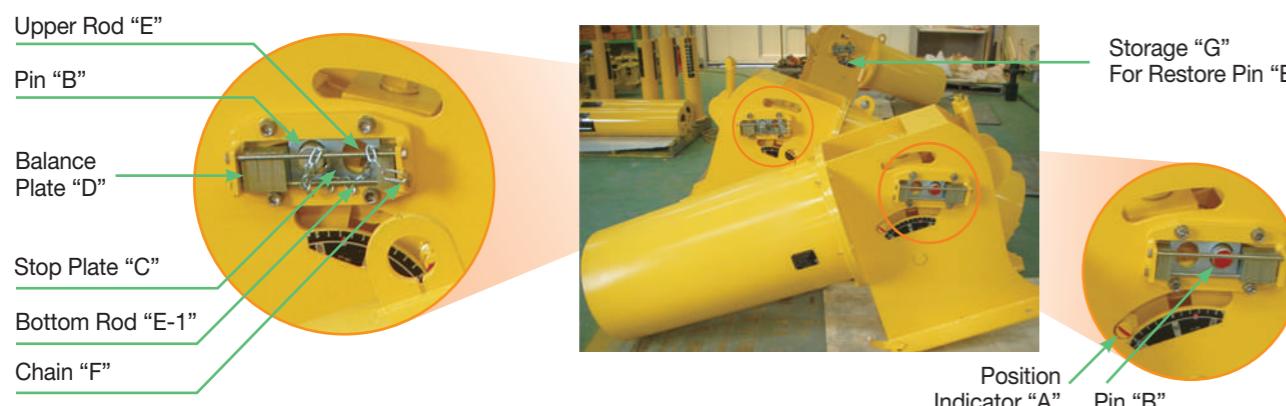
<Sequence>

1. Release the Upper Rod "E" (Not release the Bottom Rod "E-1").

2. Remove(Pulling) the Pin "B"

3. Restore the removed The Pin "B" in the Storage "G"

4. Reassembly the Upper Rod "E"



* from Installation to Operation



MAINTENANCE & RESETTING MANUAL

* Maintenance

1. Each Spring hanger should be periodically inspected visually to verify the correct setting of the position indicator during operation.

2. Inspection frequency may be at each scheduled plant shut-down and annual inspection, at least recommended.

3. All dust, soot and foreign objects which may impair hanger operation shall be removed.

4. Observe and record the position of the position indicator once a year in hot and cold states and when unexpected movement has been detected, the cause must be investigated.

5. Loose or fallen nuts should be tightened.

6. Damaged parts are to be repaired or replaced.

